## Servo Motor Selection Flow Chart




| Explanation | References |
| :--- | :---: |
| •Calculate Regenerative Energy from the <br> Torque of all the moving parts. | •Please see the user manual <br> of each product for the details <br> on calculation of the <br> regenerative energy. |
| -Check if the the number of encoder pulses <br> meets the system specified resolution. | •Accuracy of Positioning |
| -Check if the calculation meets the <br> specifications of the temporarily selected <br> motor. <br> If not, change the temporarily selected motor <br> and re-calculate it. | •The following table |


| Specialized Check Items | Check Items |
| :---: | :---: |
| Load Inertia | Load Inertia $\leq$ Motor Rotor Inertia x Applicable Inertia Ratio |
| Effective Torque | Effective Torque < Motor Rated Torque <br> - Please allow a margin of about 20\%. * |
| Maximum <br> Momentary Torque | Maximum Momentary Torque < Motor Maximum <br> Momentary Torque <br> - Please allow a margin of about $20 \%$. * <br> - For the motor Maximum Momentary Torque, use the value that is combined with a driver and the one of the motor itself. |
| Maximum Rotation Speed | Maximum Rotation Speed $\leq$ Rated Rotation Speed of a motor <br> - Try to get as close to the motor's rated rotations as possible. It will increase the operating efficiency of a motor. <br> - For the formula, please see "Straight-line Speed and Motor Rotation Speed" on Page 11. |
| Regenerative Energy | Regenerative Energy $\leq$ Regenerative Energy Absorption of a motor <br> -When the Regenerative Energy is large, connect a Regenerative Energy Absorption Resistance to increase the Absorption capacity of the driver. |
| Encoder Resolution | Ensure that the Encoder Resolution meets the system specifications. |
| Characteristics of a Positioner | Check if the Pulse Frequency does not exceed the Maximum Response Frequency or Maximum Command Frequency of a Positioner. |
| Operating Conditions | Ensure that values of the ambient operating temperature/ humidity, operating atmosphere, shock and vibrations meet the product specifications. |

* When handling vertical loads and a load affected by the external torque, allow for about 30\% of capacity.


## Formulas

■Formulas for Operating Patterns
Sriangular
Speed and Slope

■Inertia Formulas

| Cylindrical Inertia |  | $J_{w}=\frac{M\left(D_{1}^{2}+D_{2}^{2}\right)}{8} \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| :---: | :---: | :---: |
| Eccentric Disc Inertia (Cylinder which rotates off the center axis) |  | $J_{w}=J_{C}+M \cdot r \mathrm{e}^{2} \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| Inertia of Rotating Square Cylinder | M: Square Cylinder Mass (kg) | $J_{w}=\frac{M\left(a^{2}+b^{2}\right)}{12} \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| Inertia of Linear Movement |  | $\mathrm{J}_{\mathrm{w}}=\mathrm{M}\left(\frac{\mathrm{P}}{2 \pi}\right)^{2} \times 10^{-6}+\mathrm{J}_{\mathrm{B}}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| Inertia of Lifting Object by Pulley | D: Diameter (mm) <br> $\mathrm{M}_{1}$ : Mass of Cylinder (kg) <br> $J_{1}$ : Cylinder Inertia $\left(\mathrm{kg} \cdot \mathrm{m}^{2}\right)$ <br> $\mathrm{J}_{2}$ : Inertia due to the Object $\left(\mathrm{kg} \cdot \mathrm{m}^{2}\right)$ <br> $\mathrm{M}_{2}$ : Mass of Object (kg) <br> $\mathrm{J}_{\mathrm{w}}$ : Inertia (kg•m²) | $\begin{aligned} J_{w} & =J_{1}+J_{2} \\ & =\left(\frac{M_{1} \cdot D^{2}}{8}+\frac{M_{2} \cdot D^{2}}{4}\right) \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right) \end{aligned}$ |


| Inertia of Rack and Pinion Movement |  | $J_{w}=\frac{M \cdot D^{2}}{4} \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| :---: | :---: | :---: |
| Inertia of Suspended Counterbalance |  | $J_{W}=\frac{D^{2}\left(M_{1}+M_{2}\right)}{4} \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| Inertia when Carrying Object via Conveyor Belt |  | $\begin{aligned} & J_{W}= J_{1}+J_{2}+J_{3}+J_{4} \\ &=\left(\frac{M_{1} \cdot D_{1}^{2}}{8}+\frac{M_{2} \cdot D_{2}^{2}}{8} \cdot \frac{D_{1}^{2}}{D_{2}^{2}}+\right. \\ &\left.\frac{M_{3} \cdot D_{1}^{2}}{4}+\frac{M_{4} \cdot D_{1}^{2}}{4}\right) \times 10^{-6} \\ &\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right) \end{aligned}$ |
| Inertia where Work is Placed between Rollers | $\mathrm{J}_{\mathrm{w}}$ : System Inertia (kg•m²) <br> $J_{1}$ : Roller 1 Inertia ( $\mathrm{kg} \cdot \mathrm{m}^{2}$ ) <br> $J_{2}$ : Roller 2 Inertia (kg•m²) <br> $\mathrm{D}_{1}$ : Roller 1 Diameter (mm) <br> $\mathrm{D}_{2}$ : Roller 2 Diameter (mm) <br> M : Equivalent Mass of Work (kg) | $J_{W}=J_{1}+\left(\frac{D_{1}}{D_{2}}\right)^{2} J_{2}+\frac{M \cdot D_{1}{ }^{2}}{4} \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| Inertia of a Load Value Converted to Motor Shaft |  | $J_{L}=J_{1}+\mathrm{G}^{2}\left(\mathrm{~J}_{2}+J_{\mathrm{W}}\right)\left(\mathrm{kg} \cdot \mathrm{m}^{2}\right)$ |

## ■Load Torque Formulas

| Torque against external force |  | $\mathrm{T}_{\mathrm{W}}=\frac{\mathrm{F} \cdot \mathrm{P}}{2 \pi} \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| :---: | :---: | :---: |
| Torque against frictional force | M: Load Mass (kg) | $\mathrm{T}_{\mathrm{w}}=\mu \mathrm{Mg} \cdot \frac{\mathrm{P}}{2 \pi} \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| Torque when external force is applied to a rotating object | D: Diameter (mm) <br> F: External <br> Force (N) | $\mathrm{T}_{\mathrm{w}}=\mathrm{F} \cdot \frac{\mathrm{D}}{2} \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| Torque of an object on the conveyer belt to which the external force is applied | D: Diameter (mm) | $\mathrm{T}_{\mathrm{W}}=\mathrm{F} \cdot \frac{\mathrm{D}}{2} \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| Torque of an object to which the external force is applied by Rack and Pinion |  | $\mathrm{T}_{\mathrm{W}}=\mathrm{F} \cdot \frac{\mathrm{D}}{2} \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| Torque when work is lifted at an angle. |  | $\mathrm{T}_{\mathrm{W}}=\mathrm{Mg} \cdot \cos \theta \cdot \frac{\mathrm{D}}{2} \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| Torque of a Load Value Converted to Motor Shaft |  | $\mathrm{T}_{\mathrm{L}}=\mathrm{T}_{\mathrm{w}} \cdot \frac{\mathrm{G}}{\eta}(\mathrm{~N} \cdot \mathrm{~m})$ |

■Acceleration/Deceleration Torque Formula


## ■Calculation of Maximum Momentary Torque, Effective Torque



■Positioning Accuracy
P: Ball Screw Pitch

## ©Straight Line Speed and Motor Rotation Speed



## Sample Calculations

## (1)Machinery Selection

- Load Mass M = 5 (kg)
- Ball Screw Pitch $P=10$ (mm)
- Ball Screw Diameter D = 20 (mm)
- Ball Screw Mass $\mathrm{Mb}=3$ (kg)
- Ball Screw Friction Coefficient $\mu=0.1$
- Since there is no decelerator, $G=1, \eta=1$

(2)Determining Operating Pattern



## (3)Calculation of Motor Shaft Conversion Load Inertia

| Ball screw <br> Inertia $J_{B}$ | $J_{B}=\frac{M_{B} D^{2}}{8} \times 10^{-6}$ | $J_{B}=\frac{3 \times 20^{2}}{8} \times 10^{-6}=1.5 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| :--- | :--- | :--- |
| Load <br> Inertia $J_{w}$ | $J_{W}=M\left(\frac{P}{2 \pi}\right)^{2} \times 10^{-6}+J_{B}$ | $J_{W}=5 \times\left(\frac{10}{2 \times 3.14}\right)^{2} \times 10^{-6}+1.5 \times 10^{-4}=1.63 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |
| Motor Shaft Conversion <br> Load Inertia $J_{L}$ | $J_{L}=G^{2} \times\left(J_{W}+J_{2}\right)+J_{1}$ | $J_{L}=J_{W}=1.63 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ |

(4)Load Torque Calculation

| Torque against Friction <br> Torque $\mathrm{T}_{\mathrm{w}}$ | $\mathrm{T}_{\mathrm{w}}=\mu \mathrm{Mg} \frac{\mathrm{P}}{2 \pi} \times 10^{-3}$ | $\mathrm{~T}_{\mathrm{W}}=0.1 \times 5 \times 9.8 \times \frac{10}{2 \times 3.14} \times 10^{-3}=7.8 \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |
| :--- | :--- | :--- |
| Motor Shaft Conversion <br> Load Torque $\mathrm{T}_{\mathrm{L}}$ | $\mathrm{T}_{\mathrm{L}}=\frac{\mathrm{G}}{\mathrm{n}} \cdot \mathrm{T}_{\mathrm{W}}$ | $\mathrm{T}_{\mathrm{L}}=\mathrm{T}_{\mathrm{W}}=7.8 \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |

## (5)Calculation of Rotation Speed

| Rotations $\mathbf{N}$ | $\mathrm{N}=\frac{60 \mathrm{~V}}{\mathrm{P} \cdot \mathrm{G}}$ | $\mathrm{N}=\frac{60 \times 300}{10 \times 1}=1800(\mathrm{r} / \mathrm{min})$ |
| :--- | :--- | :--- |

(6)Motor Temporary Selection [In case OMNUC U Series Servo Motor is temporarily selected]

| The Rotor/Inertia of the <br> selected servo motor is <br> more than $1 / 30^{*}$ of a load | $\mathrm{JM} \geq \frac{\mathrm{J}_{\mathrm{L}}}{30}$ | $\frac{\mathrm{J}_{\mathrm{L}}}{30}=\frac{1.63 \times 10^{-4}}{30}=5.43 \times 10^{-6}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ <br> Temporarily selected Model R88M $-\mathrm{U} 20030\left(\mathrm{~J}_{\mathrm{M}}=1.23 \times 10^{-5}\right)$. |
| :--- | :--- | :--- |
| $80 \%$ of the Rated Torque <br> of the selected servo <br> motor is more than the <br> load torque of the <br> servomotor shaft <br> conversion value | $\mathrm{T}_{\mathrm{M}} \times 0.8>\mathrm{T}_{\mathrm{L}}$ | Rated Torque for R88M -U 20030 Model from TM $=0.637(\mathrm{~N} \cdot \mathrm{~m})$ <br> $T_{M}=0.637(\mathrm{~N} \cdot \mathrm{~m}) \times 0.8>\mathrm{T}_{\mathrm{L}}=7.8 \times 10^{-3}(\mathrm{~N} \cdot \mathrm{~m})$ |

[^0]
## (7)Calculation of Acceleration/Deceleration Torque

| Acceleration/ <br> Deceleration Torque $T_{A}$ | $T_{A}=\frac{2 \pi \cdot N}{60 t_{A}}\left(J_{M}+\frac{J_{L}}{\eta}\right)$ | $T_{A}=\frac{2 \pi \times 1800}{60 \times 0.2} \times\left(1.23 \times 10^{-5}+\frac{1.63 \times 10^{-4}}{1.0}\right)=0.165(\mathrm{~N} \cdot \mathrm{~m})$ |
| :--- | :--- | :--- |

## (8)Calculation of Maximum Momentary Torque, Effective Torque

## Required Max. Momentary Torque is

$$
\begin{aligned}
& \mathrm{T}_{1}=\mathrm{T}_{\mathrm{A}}+\mathrm{T}_{\mathrm{L}}=0.165+0.0078 \\
&=0.173(\mathrm{~N} \cdot \mathrm{~m}) \\
& \mathrm{T}_{2}=\mathrm{T}_{\mathrm{L}}=0.0078(\mathrm{~N} \cdot \mathrm{~m}) \\
& \mathrm{T}_{3}=\mathrm{T}_{\mathrm{L}}-\mathrm{T}_{\mathrm{A}}=0.0078-0.165 \\
&=-0.157(\mathrm{~N} \cdot \mathrm{~m})
\end{aligned}
$$

Effective Torque Trms is
Trms $=\sqrt{\frac{T_{1}{ }^{2} \cdot t_{1}+T_{2}{ }^{2} \cdot t_{2}+T_{3}{ }^{2} \cdot t_{3}}{t_{1}+t_{2}+t_{3}+t_{4}}}$
$=\sqrt{\frac{0.173^{2} \times 0.2+0.0078^{2} \times 1.0+0.157^{2} \times 0.2}{0.2+1.0+0.2+0.2}}$
$=0.0828(\mathrm{~N} \cdot \mathrm{~m})$


## Result of Examination

| Load Inertia | [Load Inertia JL $=1.63 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ ] <br> $\leq$ [Motor Rotor Inertia $\left.\mathrm{Jm}=1.23 \times 10^{-5}\right] \times$ [Applied Inertia $\left.=30\right]$ | Conditions Satisfied |
| :---: | :---: | :---: |
| Effective Torque | [Effective Torque Trms $=0.0828(\mathrm{~N} \cdot \mathrm{~m})$ ] < [Servomotor Rated Torque $0.637(\mathrm{~N} \cdot \mathrm{~m}) \times 0.8$ ] | Conditions Satisfied |
| Maximum Momentary Torque | [Maximum Momentary Torque $\mathrm{T}_{1}=0.173 \mathrm{~N} \cdot \mathrm{~m}<$ [Servomotor Maximum Momentary Torque $1.91(\mathrm{~N} \cdot \mathrm{~m}) \times 0.8$ ] | Conditions Satisfied |
| Maximum Rotation Speed | [Maximum Rotations Required $\mathrm{N}=1800$ (r/min)] $\leq$ [Servomotor Rated Rotation Speed 3000 (r/min)] | Conditions Satisfied |
| Encoder Resolution | The encoder resolution when the positioner multiplication factor is set to 1 is $\mathrm{R}=\frac{\mathrm{P} \cdot \mathrm{G}}{\mathrm{Ap} \cdot \mathrm{~S}}=\frac{10 \times 1}{0.01 \times 1}=1000 \text { (Pulses/Rotations) }$ <br> The encoder specification of U Series 2048 (pulses/rotation) should be set 1000 with the Encoder Dividing Rate Setting. | Conditions Satisfied |

Note.This example omits calculations for the regenerative energy, operating conditions, or positioner characteristics.


[^0]:    * Note that this value changes according to the Series.

